

INTERNATIONAL CONFERENCE  
St Petersburg, RUSSIA  
04 March 20120



# «Metrological Support of Innovative Technologies» ICMSIT-2020

«Plastic bending of the waveguide tubes with rectangular cross-section»

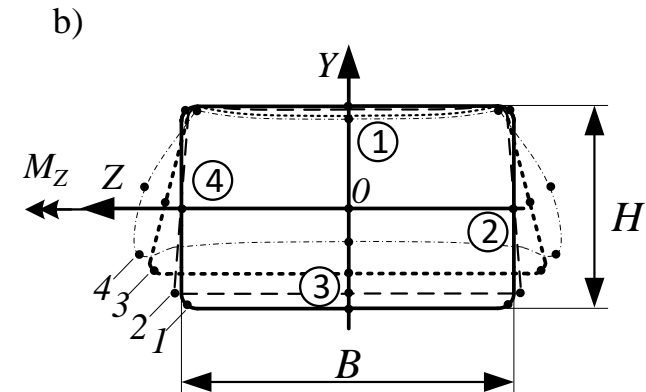
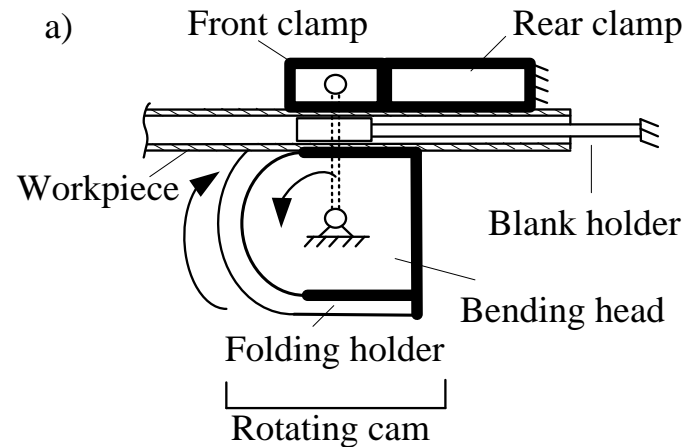
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# Problem statement

- Problems of manufacturing curved waveguide sections on the tube-bending machine:
- undesirable deformations of a cross-section;
- unacceptable thinning, cracks and wrinkles;
- limited angles and radii of bending.



Plastic bending process on the tube-bending machine



# Solution methods

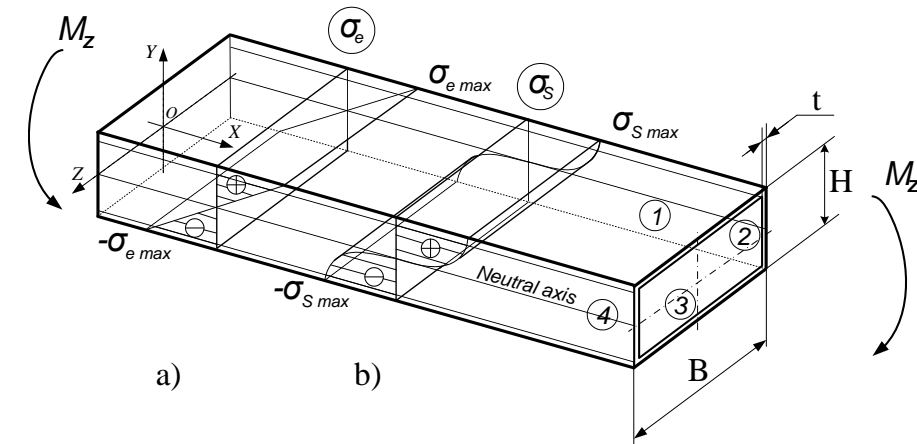
- Rectilinear waveguide is modelled by the theory of shells as composite construction which consist of 4 plates
- Complete system of the waveguide constitutive equations consists of 4 subsystems for each of its plates and have the form of nonlinear partial differential equations

- constitutive equations

$$\left. \begin{aligned} \frac{\partial^4 \varphi_i}{\partial \alpha_i^4} + 2 \frac{\partial^4 \varphi_i}{\partial \alpha_i^2 \partial \beta_i^2} + \frac{\partial^4 \varphi_i}{\partial \beta_i^4} &= Et \cdot \left[ \left( \frac{\partial^2 \omega_i}{\partial \alpha_i \partial \beta_i} \right)^2 - \frac{\partial^2 \omega_i}{\partial \alpha_i^2} \cdot \frac{\partial^2 \omega_i}{\partial \beta_i^2} \right]; \\ \frac{\partial^4 \omega_i}{\partial \alpha_i^4} + 2 \frac{\partial^4 \omega_i}{\partial \alpha_i^2 \partial \beta_i^2} + \frac{\partial^4 \omega_i}{\partial \beta_i^4} &= \frac{1}{D} \left[ \frac{\partial^2 \varphi_i}{\partial \beta_i^2} \cdot \frac{\partial^2 \omega_i}{\partial \alpha_i^2} - 2 \frac{\partial^2 \varphi_i}{\partial \alpha_i \partial \beta_i} \cdot \frac{\partial^2 \omega_i}{\partial \alpha_i \partial \beta_i} + \frac{\partial^2 \varphi_i}{\partial \alpha_i^2} \cdot \frac{\partial^2 \omega_i}{\partial \beta_i^2} \right]. \end{aligned} \right\}$$

- analytic solution

$$\left. \begin{aligned} \varphi_1 &= \beta_1^2 \cdot \frac{M_z}{J_z} \cdot \frac{h'}{4}; & w_1 &= \frac{h'}{2} - \frac{M_z}{2 \cdot EJ_z} \left[ \alpha_1^2 + \mu \cdot \frac{h'^2}{4} \right]; & \varphi_2 &= \frac{M_z}{J_z} \cdot \frac{\beta_2^3}{6}; & w_2 &= 0; \\ \varphi_3 &= -\beta_3^2 \cdot \frac{M_z}{J_z} \cdot \frac{h'}{4}; & w_3 &= -\frac{h'}{2} + \frac{M_z}{2 \cdot EJ_z} \left[ \alpha_3^2 + \mu \cdot \frac{h'^2}{4} \right]; & \varphi_4 &= -\frac{M_z}{J_z} \cdot \frac{\beta_4^3}{6}; & w_4 &= 0. \end{aligned} \right\}$$



Stress distribution by volume of the waveguide at bending

# Conclusions

## Results, implementation

- The most critical factor limiting the value of the minimum radius of bending from below is not stress, but the value of the maximum permissible deformation of the waveguide material .
- When using a filler the thinning of the waveguide wall increases by 30-50% .
- Heating increases plastic properties of the material only by 10%.
- Superplasticity is the best method to improve bending process.

# Contacts

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