

# VIRTUAL NOX-EMISSION SENSORS FOR ROBUST AEROENGINE AUTOMATIC CONTROL SYSTEM

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## The relevance and purpose of the study

**Built-in mathematical models** of an object are actively used in modern robust control systems to implement target functions and control parameters that cannot be directly measured. This is applied particularly to NO<sub>x</sub> and CO emissions (nitrogen and carbon oxides). Meanwhile, emission levels in modern gas turbine engines are no less significant than thrust (power) performance or an engine life.

**Low-emission combustion systems** have a narrow operating range that on the one hand is restricted by a regulated level of NO<sub>x</sub> emission, and on the other hand, by a flame blow-out or high combustion dynamics (thermal acoustic natural vibrations) which are not acceptable in the field operation. Hazardous emission (primarily, NO<sub>x</sub>) for the new generation engines becomes an equally important parameter as an engine thrust. All other requirements are unconditionally met. So it is necessary to arrange both a system for continuous monitoring of emissions according to engine parameters, and the control over the combustor diffusion circuit to ensure a target level of emission (not exceeding the regulations).

**The target** NO<sub>x</sub> emission indication is its integral nature, i.e. the number of emissions per TOL (take-off and landing) cycle within the flight altitude up to 1000meters. Therefore, it is advisable to choose Climbing as an emission tuning mode based on the following considerations:

- Climbing contributes significantly to emissions thanks to a combination of a high power (85% of maximum thrust) and the engine runtime (up to 2.2 minutes). Climbing is not critical (compared to Take-Off) in terms of the flight safety.
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## The problems and purpose of the study

### Problems:

- there is no existing on-board emission sensor;
- functionally the emission level depends on a large number of variables (at least six to seven);
- the low emission combustor stability margin (from lean blow-out to high combustion dynamics) depends on many parameters, and the extension of the safe envelope (where required) by increasing fuel flow through the diffusion circuit results in higher emission;
- it is necessary to take into account the NO<sub>x</sub> emission standards for the low emission combustor

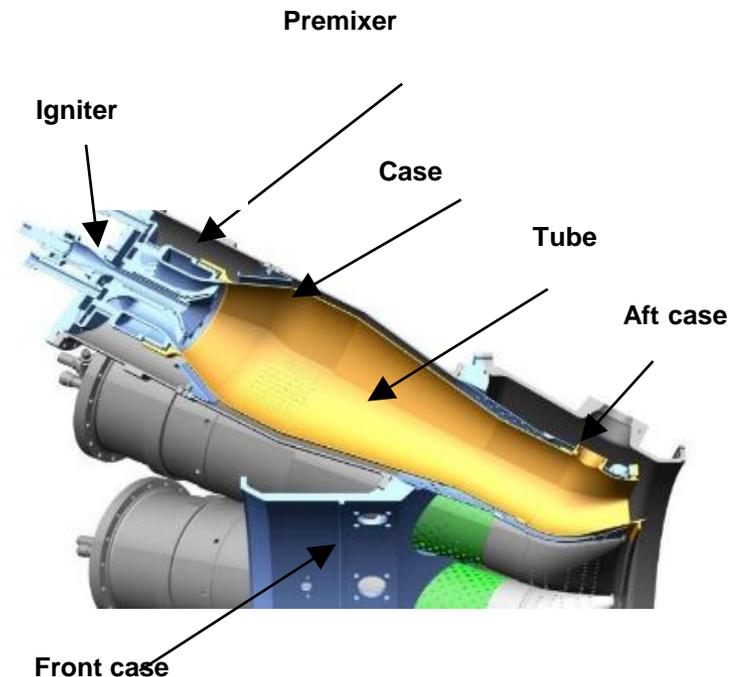
### Purpose :

The development of a virtual sensor of the emission of nitrogen oxide, built into the diffusion flame tracking automatic control system.

# RESEARCH OBJECT: THE LOW EMISSION COMBUSTION CHAMBER

## Structure:

- Front-mounted device with a blade swirl and nozzle and four fuel metering devices (diffusion and homogeneous), which function are injection, evaporation and uniform mixing of the air-fuel mixture due to transverse concentration pulsations (homogeneous collectors) and flame stability (diffusion circuit with flow rate up to 30% of total fuel consumption).
- The combustion space where the combustion process is carried out. The length of the furnace space is determined by the residence time of the mixture required to complete the combustion.



# MATHEMATICAL MODEL OF EMISSION BASED ON ZELDOVICH EQUATION

**Zeldovich equation** is taken as a mathematical model for NO<sub>x</sub> generation:

$$S = 2 \cdot 1.8 \cdot 10^8 \cdot e^{-38370/T} \cdot [O] \cdot [N_2]$$

where  $S$  -the speed(rate) of the NO<sub>x</sub> generation [mol/(m<sup>3</sup>·s)],  $T$  - temperature of flame [K],  $[O]$  - oxygen concentration,  $[N_2]$  - nitrogen concentration.

The superposition of premix and diffusion flames progresses as follows based on the assumption of their independence in a spacial position. Using the probability addition theorem, we place the characteristics of flames stochastic in terms of a mixture composition on one of the. Here, it's convenient to choose a fuel-air equivalence ratio  $\phi$  as an argument. Then the stable combustion range is  $\phi = 0.15 \dots 2.0$ . An increase in the argument corresponds to the increase in the proportion of the fuel flow.

The equation of the fuel flow ( $m_f$ ) averaged NO<sub>x</sub> generation rate for a typical two-zone (diffusion flame with 'd' index and homogeneous or technically premixed flame, with 'h' index) for the low emission combustor with 10:90 %% fuel split at Maximum can be represented as:

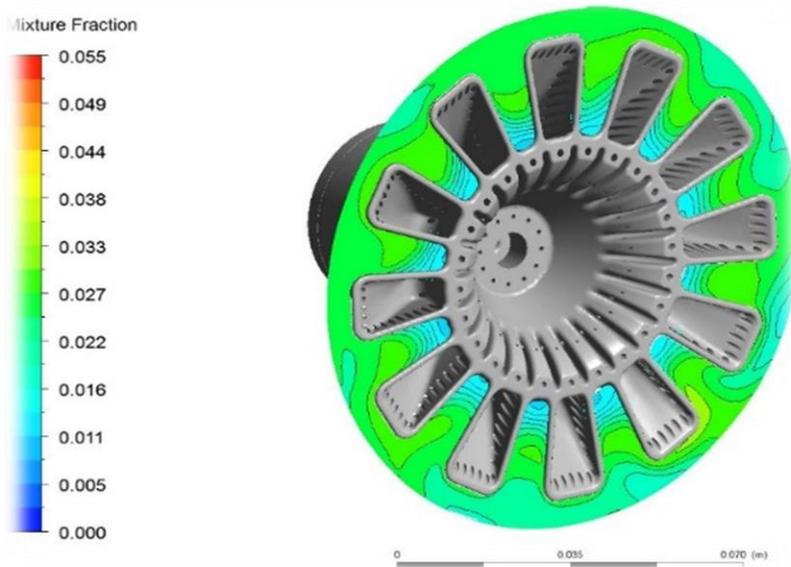
$$\bar{S} = \int_0^{0.1} S(\bar{\phi}_d, \bar{\phi}_d^{r2}) P(\phi) d\phi + \int_{0.1}^1 S(\bar{\phi}_h, \bar{\phi}_h^{r2}) P(\phi) d\phi$$

where  $S$  -the rate of the NO<sub>x</sub> generation,  $P$ - probability,  $\phi$  -equivalence ratio, is the prediction of the mathematical expectation of an equivalence ratio in diffusion and homogeneous flames; is the dispersion of the equivalent mixture ratio in diffusion and homogeneous flames with taking into account heterogeneity in a fuel flow, harmonic longitudinal acoustic pulsation of a flow and background turbulence.

# THE RESULTS OF THE NUMERIC ANALYSIS OF NON-UNIFORMITY AND THE COMBUSTION DYNAMICS DISTRIBUTION

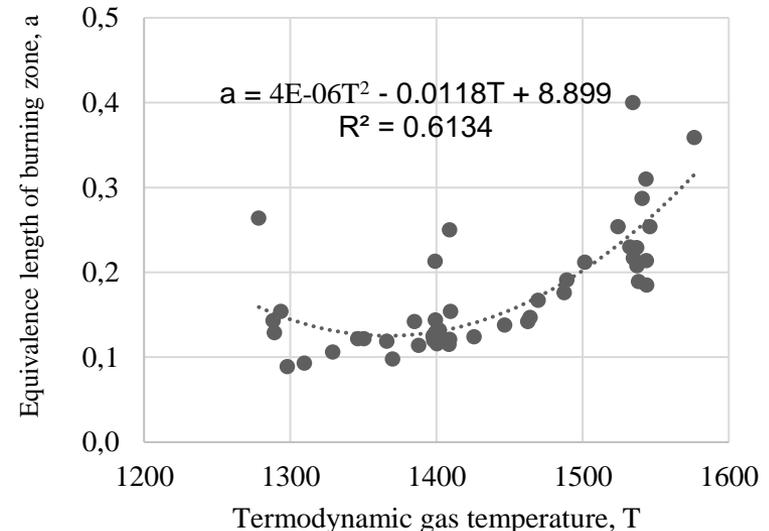
The distribution of a mixture fraction after premixer (inlet in burning zone)

The approximation of experimental data using a presented model



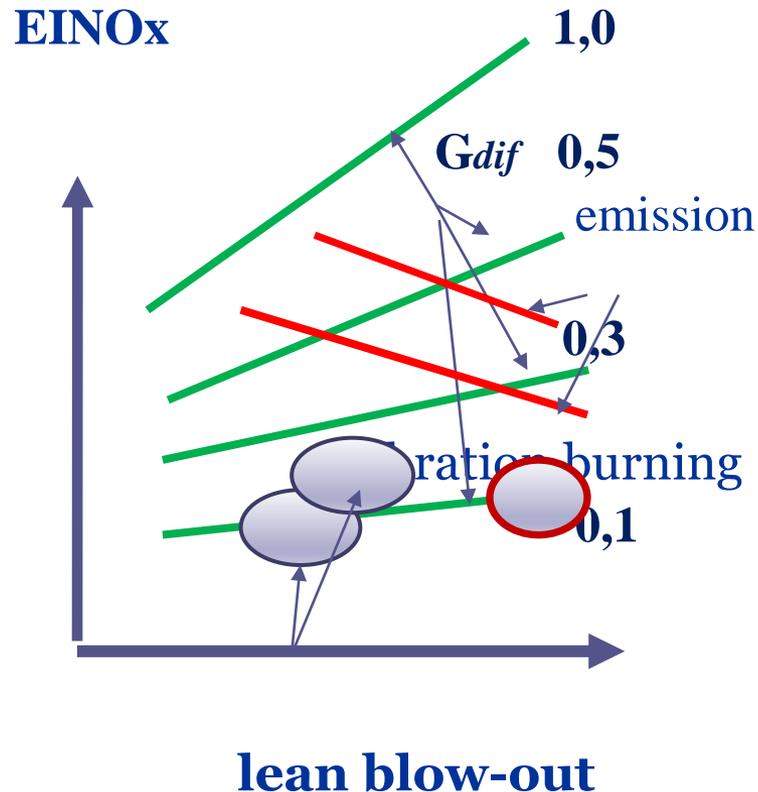
Mixture fraction was obtained on the metamodel using ANSYS CFX. For the concentration of the fuel-air mixture over the area of the premix flame were used as inputs. The standard deviation from the mathematical expectation was 15%.

Taking into account the assumptions made and NOx emission index test results, the equivalence length of burning zone (parameter “a”) was determined as a function of thermodynamic gas temperature at combustor discharge. The values of NOx emission index can be predicted using the discussed approach with no exceeding 10...20% error.



# STATEMENT OF THE CONTROL PROBLEM

## The characteristic of low-emission combustion chamber (DLN)



## The objective function

$$\int_0^t EINO_x m_f dt < [NO_x]$$

$$EINO_x \approx \mu_{NO_x} \bar{S} \frac{V}{L} \frac{a}{m_f}$$

where:

$EINO_x$  - NOx emission index [g/kg],  
 $[NO_x]$  - NOx concentration,

$a$  - equivalence length of burning zone [m],

$L$  - combustor length [m],

$m_f$  - mass fuel flow [kg/s],

$\mu$  - molar mass [g/mol],

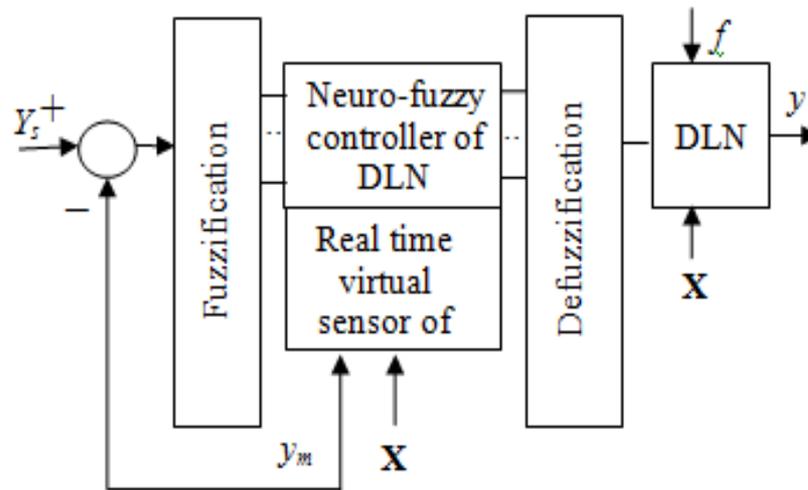
$V$  - combustor volume [m<sup>3</sup>]

**The task of an emission control** is to minimize the proportion of the fuel consumption through the diffusion circuit, taking into account the stability limitations of the combustion process in a wide range changing of external and internal factors

# THE NONLINEAR CONTROLLER WITH MATHEMATICAL MODEL BASED ON THE NEURAL NETWORK

**The main control objective function** is the minimum emission level of nitrogen and carbon oxides.

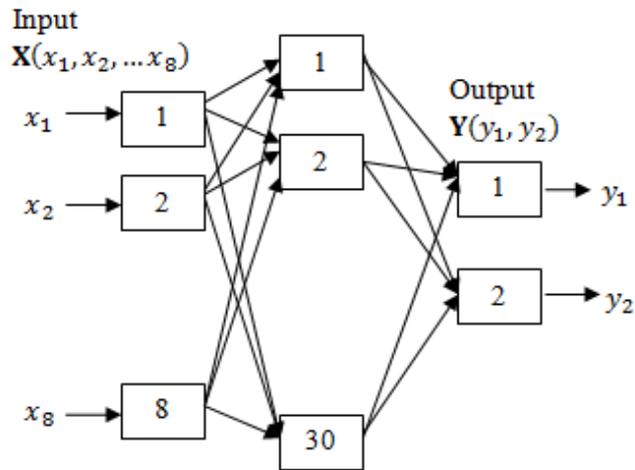
**The possible implementation of a nonlinear controller** with built-in mathematical model of the generation of NO<sub>x</sub> and CO emissions



Where:  $Y_s$  - emission target;  $y$  - real emission value;  $y_m$  - model emission value;  $f$  - disturbances (interference);  $e$  - control error;  $\mathbf{X}$  - input vector of DLN and a model of emission; DLN – dry low NO<sub>x</sub> emission combustion chamber

# MATHEMATICAL MODEL BASED ON THE NEURAL NETWORK

## The neural network structure for DLN modelling



As the coordinates of the input vector  $\mathbf{X}\{x_1, x_2, x_3, x_4, x_5, x_6, x_7, x_8\}$  the eight input parameters of DLN were selected:

- $x_1$  – operating mode;
- $x_2$  – temperature behind the compressor  $T_C$ ;
- $x_3$  – pressure behind the compressor  $P_C$ ;
- $x_4$  – air flow  $m_A$ ;
- $x_5$  – fuel flow  $m_f$ ;
- $x_6$  – gas temperature  $T_G$ ;
- $x_7$  – ripple amplitude at frequencies A200-400 Hz;
- $x_8$  – proportion of fuel in the pilot burner - pilot fuel ratio (PFR).

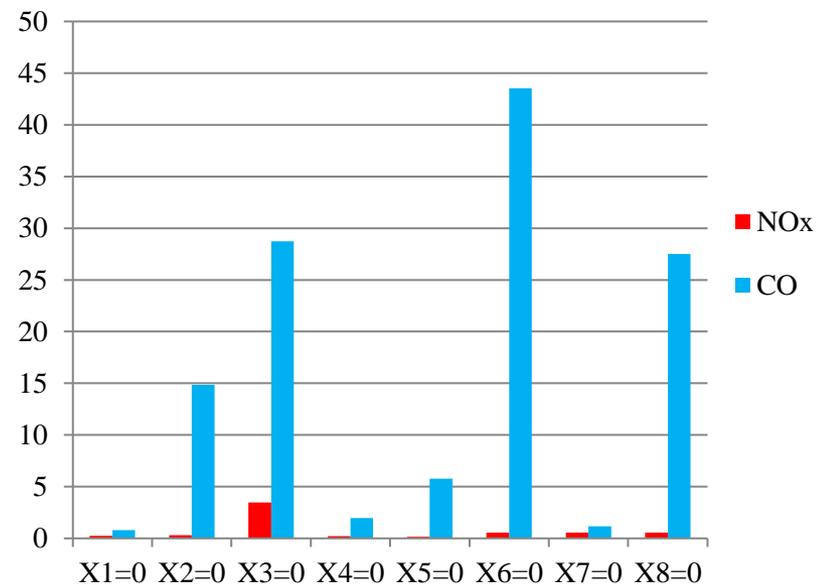
As the coordinates of the output vector of the neural network  $\mathbf{Y}(y_1, y_2)$  the two output parameters of DLN, characterizing the emission, were selected:

- $y_1$  – concentration of NO<sub>x</sub>;
- $y_2$  – concentration of CO.

The best result of neural network tunings according to the minimum of the mean square error criterion performed an average relative test error of 10%, an average relative prediction error of 3%.

By the data of a model experiment, the most significant parameters affecting the accuracy of the DLN model are the pressure behind the compressor, the gas temperature and the pilot fuel ratio (PFR).

## The results of studies of the effect of DLN input parameters on the emission of pollutants into the atmosphere



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